

Example

$$[\sigma] = \begin{bmatrix} 80 & 20 & 40 \\ 20 & 60 & 10 \\ 40 & 10 & 20 \end{bmatrix}$$

①

- ① Determine stress vector on a plane with a normal vector $\vec{R} = \hat{i} + 2\hat{j} + \hat{k}$
- ② Determine principal stresses (σ_1, σ_2 and σ_3), and τ_{max} .
- ③ Determine τ_{oct} and compare to τ_{max} .

Solution

① stress on a plane $\Rightarrow \vec{\sigma}_p = \sigma_{px} \hat{i} + \sigma_{py} \hat{j} + \sigma_{pz} \hat{k}$

$$\sigma_{px} = l\sigma_{xx} + m\sigma_{xy} + n\sigma_{xz}$$

$$\sigma_{py} = l\sigma_{xy} + m\sigma_{yy} + n\sigma_{yz}$$

$$\sigma_{pz} = l\sigma_{xz} + m\sigma_{yz} + n\sigma_{zz}$$

what are l, m, n ? \rightarrow Normalize \vec{R}

$$\text{length}(R) = \sqrt{(1)^2 + (2)^2 + (1)^2} = \sqrt{6}$$

$$\vec{R}_n = \frac{1}{\sqrt{6}} \hat{i} + \frac{2}{\sqrt{6}} \hat{j} + \frac{1}{\sqrt{6}} \hat{k}$$

$$\Rightarrow l = \frac{1}{\sqrt{6}}, \quad m = \frac{2}{\sqrt{6}}, \quad n = \frac{1}{\sqrt{6}}$$

$$\Rightarrow \sigma_{px} = \left(\frac{1}{\sqrt{6}}\right)(80) + \left(\frac{2}{\sqrt{6}}\right)(20) + \left(\frac{1}{\sqrt{6}}\right)(40) = 65.320$$

$$\sigma_{py} = \left(\frac{1}{\sqrt{6}}\right)(20) + \left(\frac{2}{\sqrt{6}}\right)(60) + \left(\frac{1}{\sqrt{6}}\right)(10) = 61.237$$

$$\sigma_{pz} = \left(\frac{1}{\sqrt{6}}\right)(40) + \left(\frac{2}{\sqrt{6}}\right)(10) + \left(\frac{1}{\sqrt{6}}\right)(20) = 32.660$$

$$\vec{\sigma}_p = 65.320 \hat{i} + 61.237 \hat{j} + 32.660 \hat{k}$$

(2) Principal stresses

②

$$\sigma^3 - I_1 \sigma^2 + I_2 \sigma - I_3 = 0$$

$$I_1 = \sigma_{xx} + \sigma_{yy} + \sigma_{zz} = 80 + 60 + 20 = 160$$

$$\begin{aligned} I_2 &= \sigma_{xx} \sigma_{yy} + \sigma_{xx} \sigma_{zz} + \sigma_{yy} \sigma_{zz} - \sigma_{xy}^2 - \sigma_{xz}^2 - \sigma_{yz}^2 \\ &= (80)(60) + (80)(20) + (60)(20) - (20)^2 - (40)^2 - (10)^2 \\ &= 5500 \end{aligned}$$

$$I_3 = \det(\sigma) = 0$$

$$\Rightarrow \sigma^3 - 160\sigma^2 + 5500\sigma = 0$$

$$\sigma_1 = 110, \quad \sigma_2 = 50, \quad \sigma_3 = 0$$

τ_{max}

$$\tau_{max} = \frac{1}{2} (\sigma_{max} - \sigma_{min}) = \frac{1}{2} (110 - 0) = 55$$

(3) τ_{oct}

$$\begin{aligned} \tau_{oct} &= \frac{1}{3} \sqrt{(\sigma_1 - \sigma_2)^2 + (\sigma_1 - \sigma_3)^2 + (\sigma_2 - \sigma_3)^2} \\ &= \frac{1}{3} \sqrt{(110 - 50)^2 + (110 - 0)^2 + (50 - 0)^2} \\ &\cong 45 \end{aligned}$$

Compare τ_{oct} to τ_{max}

$$\tau_{oct} < \tau_{max}$$

$$\Rightarrow \tau_{max} = 1.223 \tau_{oct}$$

Example For a pure Torsion problem of the bar shown

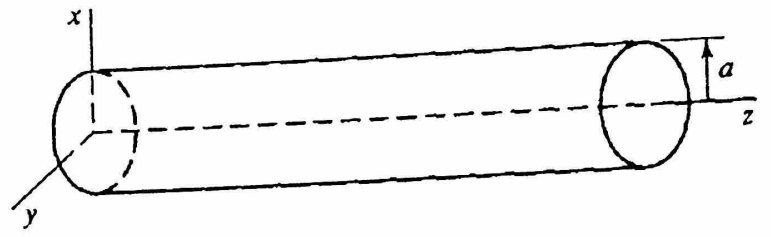
$$[\sigma] = \begin{bmatrix} 0 & 0 & -Gy\beta \\ 0 & 0 & Gx\beta \\ -Gy\beta & Gx\beta & 0 \end{bmatrix} \quad G \text{ and } \beta \text{ constants}$$

Determine

- (*) The principal stresses on lateral surface of the bar .
- (*) The principal directions = = = = = .

Solution

The lateral surface equation is an equation of a circle, as:



$$a^2 = x^2 + y^2$$

① principal stresses

$$\sigma^3 - I_1 \sigma^2 + I_2 \sigma - I_3 = 0$$

$$I_1 = \sigma_{xx} + \sigma_{yy} + \sigma_{zz} = 0$$

$$\begin{aligned}
 I_2 &= \cancel{\sigma_{xx}\sigma_{yy}} + \cancel{\sigma_{xx}\sigma_{zz}} + \cancel{\sigma_{yy}\sigma_{zz}} - \cancel{\sigma_{xy}^2} - \sigma_{xz}^2 - \sigma_{yz}^2 \\
 &= -\sigma_{xz}^2 - \sigma_{yz}^2 = -(-Gy\beta)^2 - (Gx\beta)^2 \\
 &= -G^2 y^2 \beta^2 - G^2 x^2 \beta^2 = -G^2 \beta^2 (x^2 + y^2) \\
 &= -G^2 \beta^2 a^2
 \end{aligned}$$

$$I_3 = \det(\sigma) = 0$$

$$\Rightarrow \sigma^3 - G^2 \beta^2 a^2 \sigma = 0 \Rightarrow \sigma (\sigma^2 - G^2 \beta^2 a^2) = 0$$

$$\sigma = 0, \quad \sigma^2 = G^2 \beta^2 a^2 \Rightarrow \sigma = \pm G \beta a$$

$$\sigma_1 = G \beta a, \quad \sigma_2 = 0, \quad \sigma_3 = -G \beta a$$

② principal directions, as we did before

Don't forget to normalize

$$\vec{V}_1 = -0.5 \hat{i} + 0.5 \hat{j} + \frac{1}{\sqrt{2}} \hat{k}$$

$$\vec{V}_2 = \frac{1}{\sqrt{2}} \hat{i} + \frac{1}{\sqrt{2}} \hat{j}$$

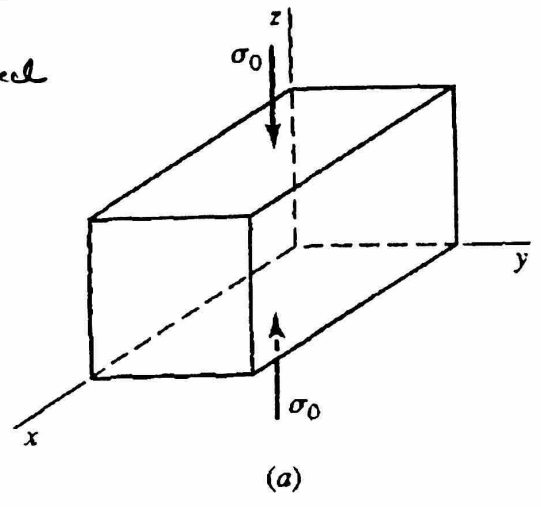
$$\vec{V}_3 = \frac{1}{2} \hat{i} - 0.5 \hat{j} + \frac{1}{\sqrt{2}} \hat{k}$$

= more details, see example 2.6 From text book

Example

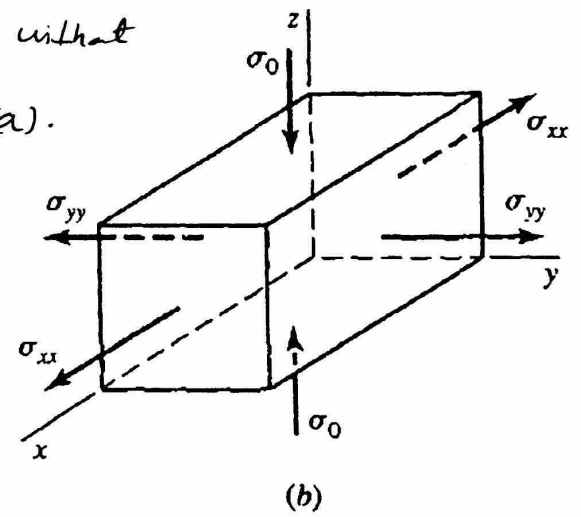
(a)

For body and loading of Figure (a)
 If Design specification says that
 the shear stress does not exceed
 160 MPa, what is the maximum
 value of σ_0 ?



(b) For figure (b), If an extra
 σ_{xx} and σ_{yy} are added in tension.

If $\sigma_{xx} > \sigma_{yy}$. Find the values of
 σ_{xx} and σ_{yy} If $\sigma_0 = 560$ MPa without
 exceeding design requirement of part (a).



(a) As shown, the body is
 principal stress state since
 that there is no shear
 stress

$$\Rightarrow \sigma_1 = \sigma_2 = 0 \quad \text{and} \quad \sigma_3 = -\sigma_0$$

Design requirement $\tau_{max} \leq 160$

$$\Rightarrow \tau_{max} = \frac{1}{2} (\sigma_{max} - \sigma_{min}) \leq 160$$

$$= \frac{1}{2} (0 - \sigma_0) \leq 160$$

$$\Rightarrow \text{Maximum allowable } \sigma_0 = +320 \text{ MPa}$$

(b) we need to find $(\sigma_{xx}, \sigma_{yy})$ while $\tau_{max} \leq 160 \text{ MPa}$ (6)
and $\sigma_0 = 560 \text{ MPa}$

Soln we are in principal stress state, so:

$$\sigma_1 = \sigma_{xx}, \quad \sigma_2 = \sigma_{yy}$$

$$\sigma_3 = \sigma_0$$

shear stresses, From 3D Mohr's circle

$$\tau_1 = \frac{1}{2} (\sigma_2 - \sigma_3)$$

$$\tau_2 = \frac{1}{2} (\sigma_1 - \sigma_3) \rightarrow \tau_{max}$$

$$\tau_3 = \frac{1}{2} (\sigma_1 - \sigma_2)$$

$$\tau_{max} = \frac{1}{2} (\sigma_{xx} - \sigma_0)$$

$$160 = \frac{1}{2} (\sigma_{xx} - 560)$$

$$320 = \sigma_{xx} - 560$$

$$\sigma_{xx} = -240 \text{ MPa}$$

let's $\tau_1 = \frac{1}{2} (\sigma_2 - \sigma_3) = \frac{1}{2} (\sigma_{yy} - \sigma_0)$

Same as above

$$\sigma_{yy} = -240 \text{ MPa}$$

